

*Brief review of building damage by the  
2011 Tohoku Japan earthquake and  
following coping activities*

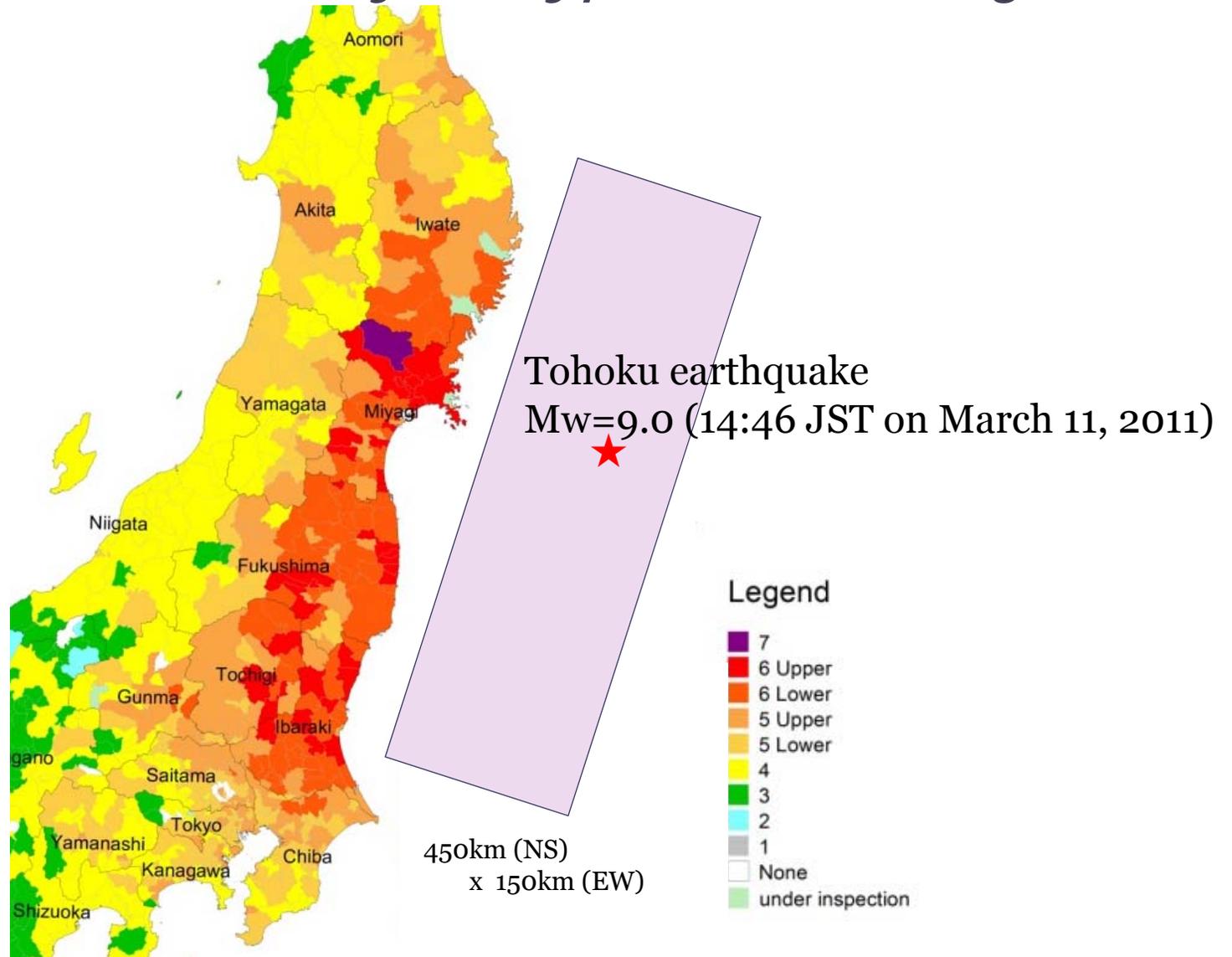
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Hiroshi Fukuyama (BRI) and Yasuo Okuda (NILIM)*

***BRI*** : Building Research Institute  
***NILIM*** : National Institute for Land & Infrastructure  
Management

*14<sup>th</sup> U.S.-Japan Workshop on Improvement of Structural Design and Construction Practices  
December 3-5, 2012, Makena Beach & Golf Resort*

# *1. Introduction*

# *JMA Seismic Intensity & Hypocentral Region*



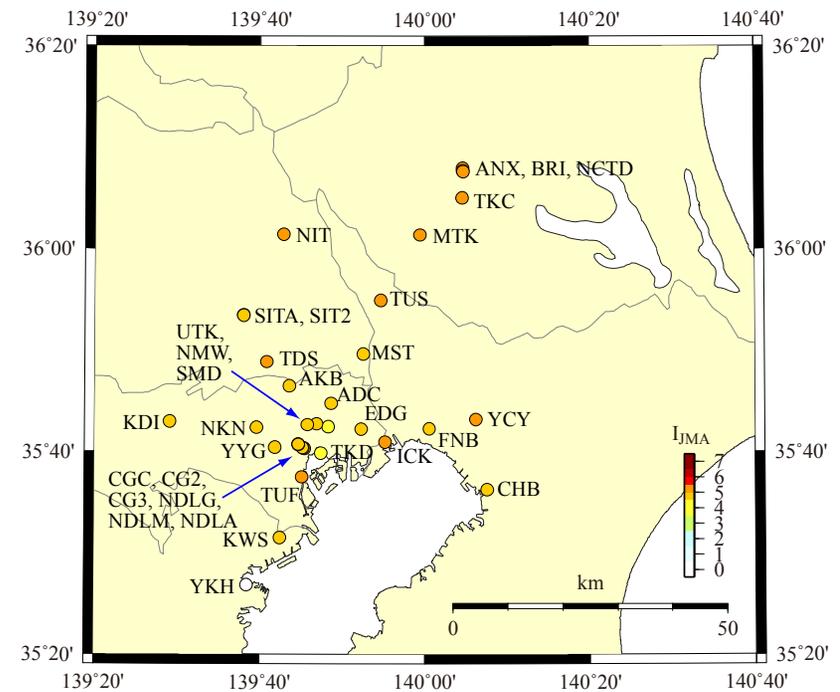
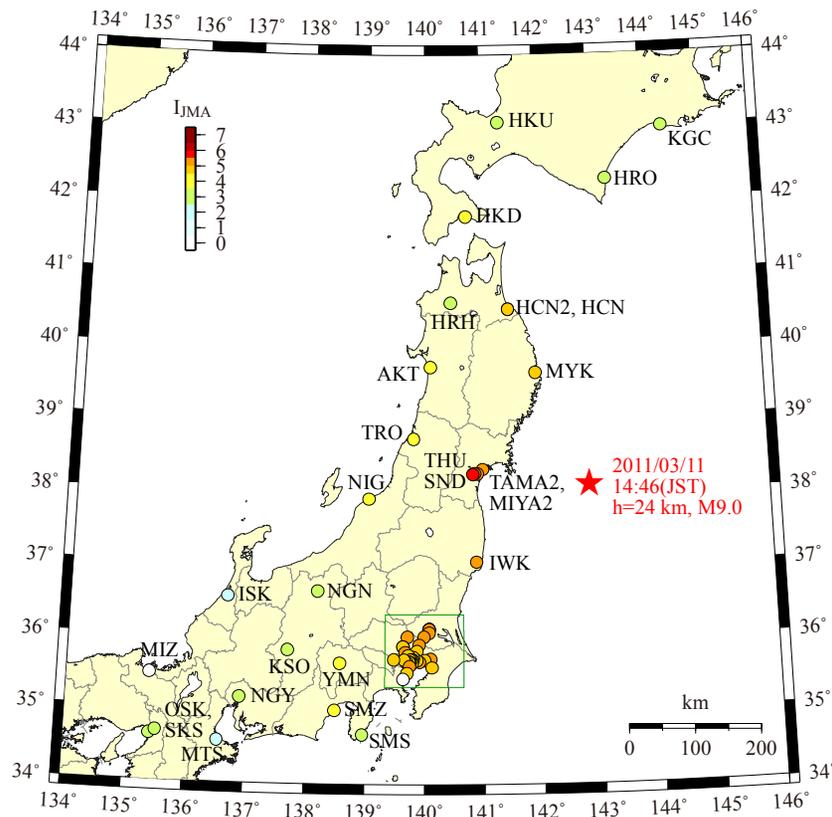
## *Building and Residential Land Damage by Earthquake Motion and Tsunami*

- *BRI and NILIM sent 43 teams for field survey and the following reports are available as of December 2, 2012*
  - <http://www.kenken.go.jp/japanese/contents/publications/data/132/index.html>
  - <http://www.kenken.go.jp/japanese/contents/publications/data/135/index.html>
  - <http://www.kenken.go.jp/japanese/contents/topics/20110311/0311report.html>
  - <http://www.kenken.go.jp/japanese/contents/publications/data/138/index.html>
  - <http://www.kenken.go.jp/english/contents/topics/20110311/0311summaryreport.html>



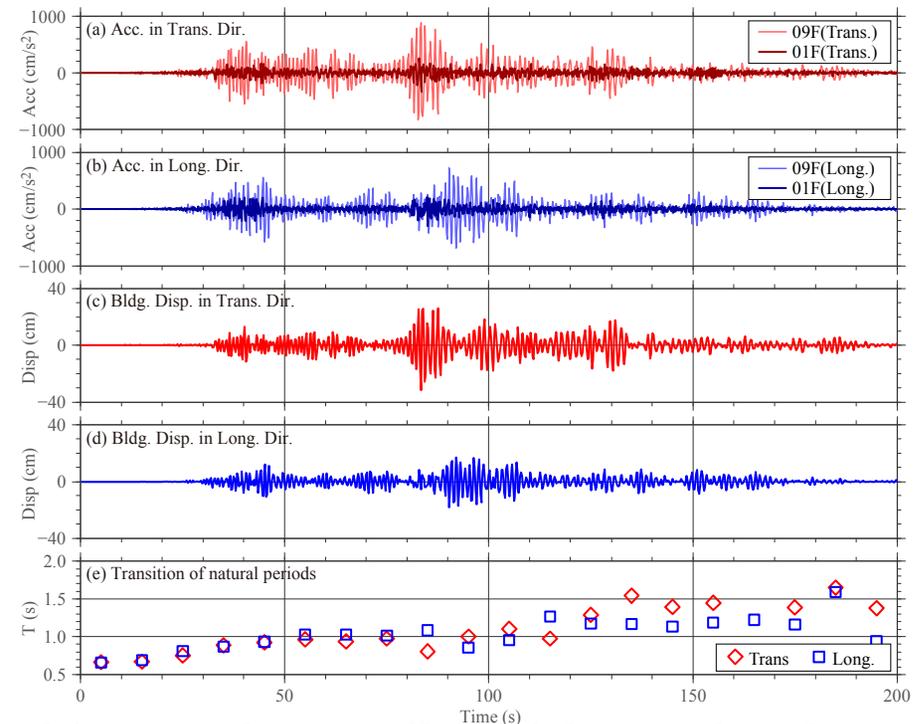
## *2. Recorded Ground and Building Motions*

# BRI Strong Motion Network



*In 1957, BRI started strong motion network.*

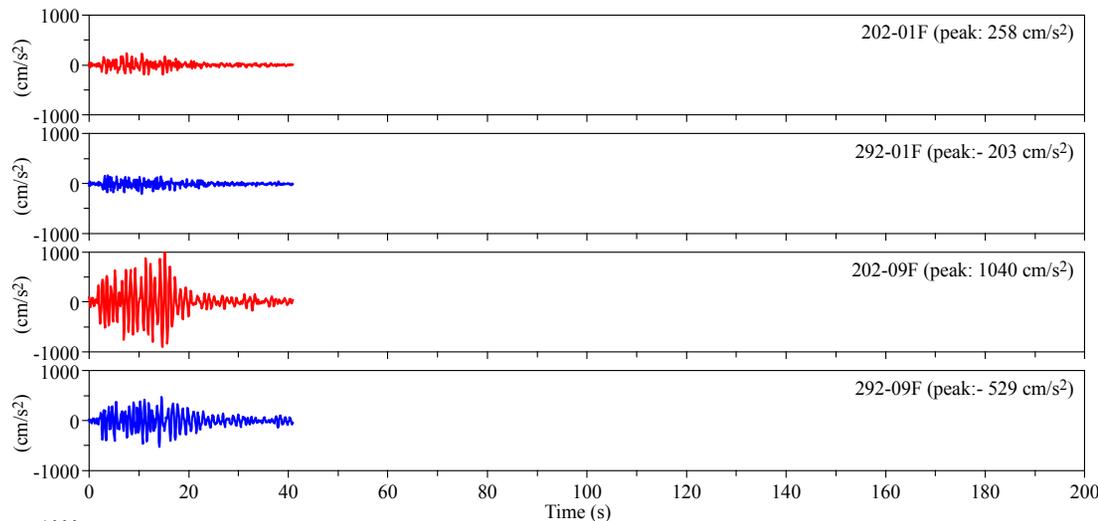
## Damaged Building in Sendai city



Flexural failure of multi-story shear walls which can absorb large earthquake energy was observed. Though the building could secure human lives by preventing its collapse as demand of seismic codes, buckling and/or rupture of steel bars and steel plates in the columns and compressive crushing of concrete were observed. Finally, the building was demolished.

## Damaged Building in Sendai city (cont.)

• 1978



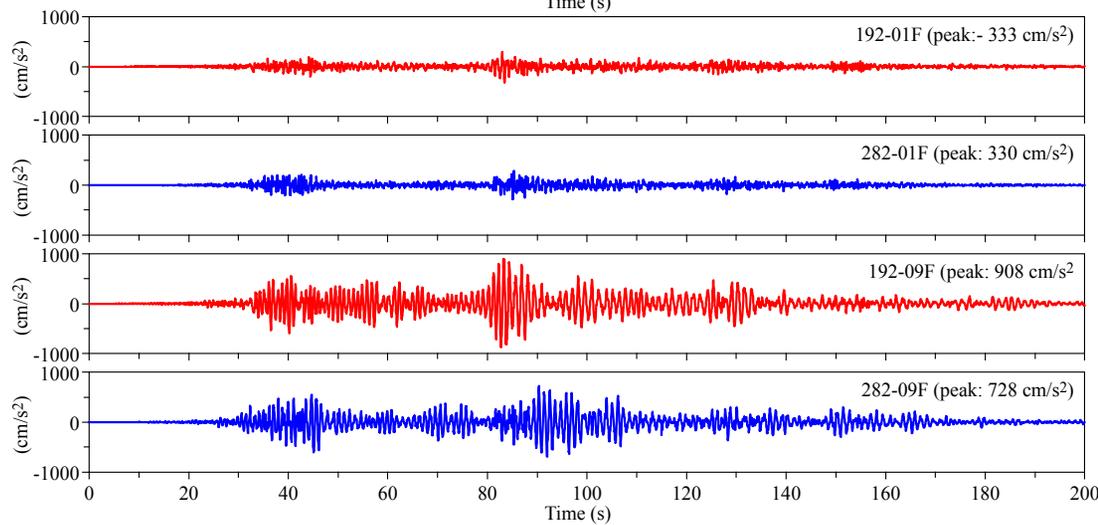
1F(NS) 258 cm/s<sup>2</sup>

1F(EW) 203 cm/s<sup>2</sup>

9F(NS) 1040 cm/s<sup>2</sup>

9F(EW) 529 cm/s<sup>2</sup>

• 2011



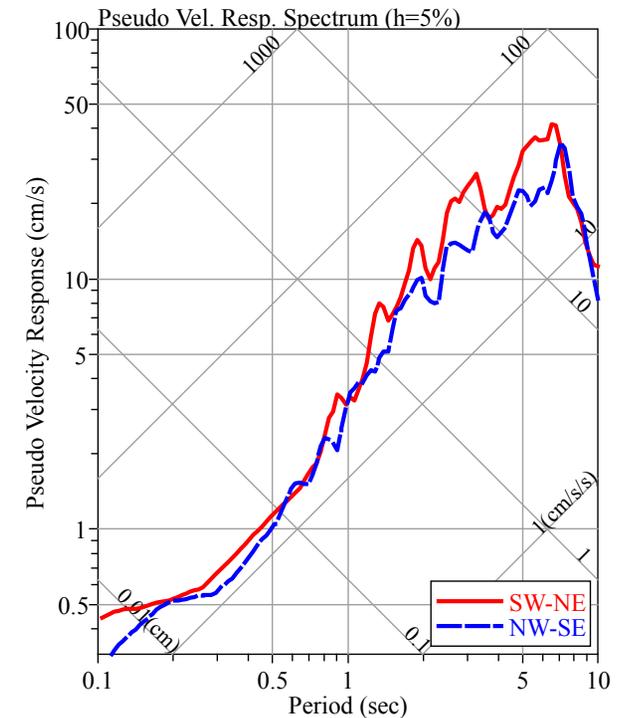
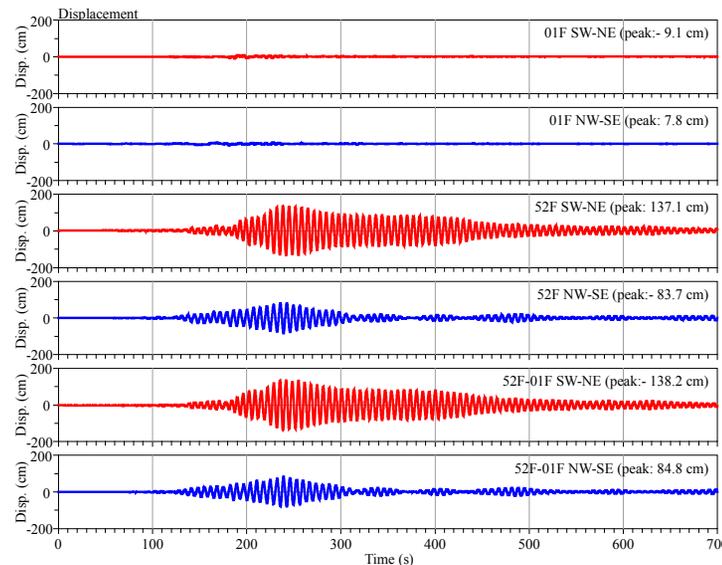
1F(NS) 333 cm/s<sup>2</sup>

1F(EW) 330 cm/s<sup>2</sup>

9F(NS) 908 cm/s<sup>2</sup>

9F(EW) 728 cm/s<sup>2</sup>

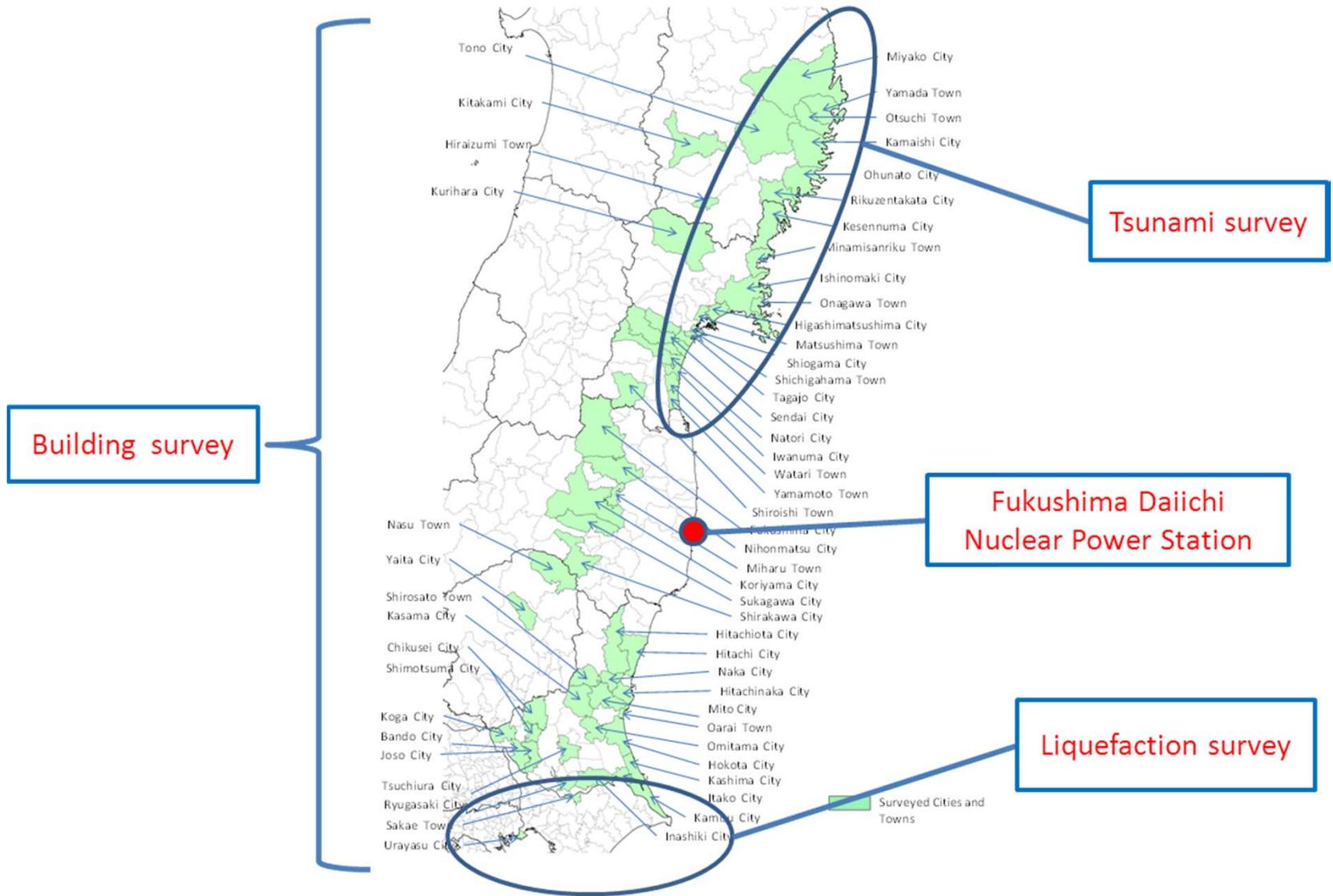
## 52+3 story building in Osaka city



- *The large responses lasted at least 10 minutes in the building in Osaka, 770km from the epicenter. A 137cm maximum displacement occurred on the top floor.*
- *Many non-structural interior members such as ceilings, walls, fire doors, sprinklers, etc. were damaged, and even confinements of passengers in elevators occurred.*

### *3. Building and Residential Land Damage*

# Field surveyed area by BRI and NILIM teams



# Earthquake Motion Damage



Courtesy to the Japan MLIT

# Earthquake Motion Damage (cont.)

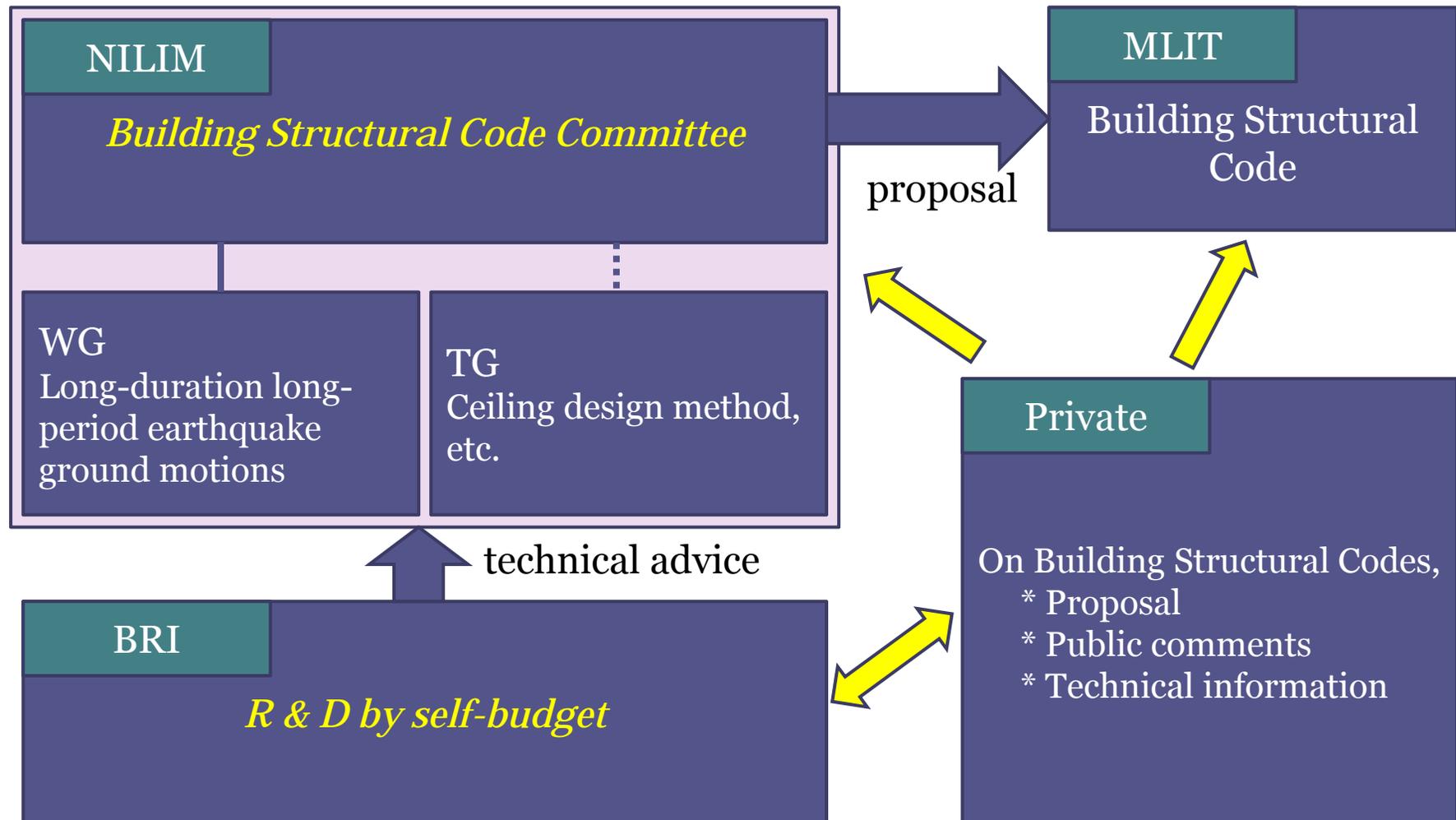


# *Tsunami Damage*



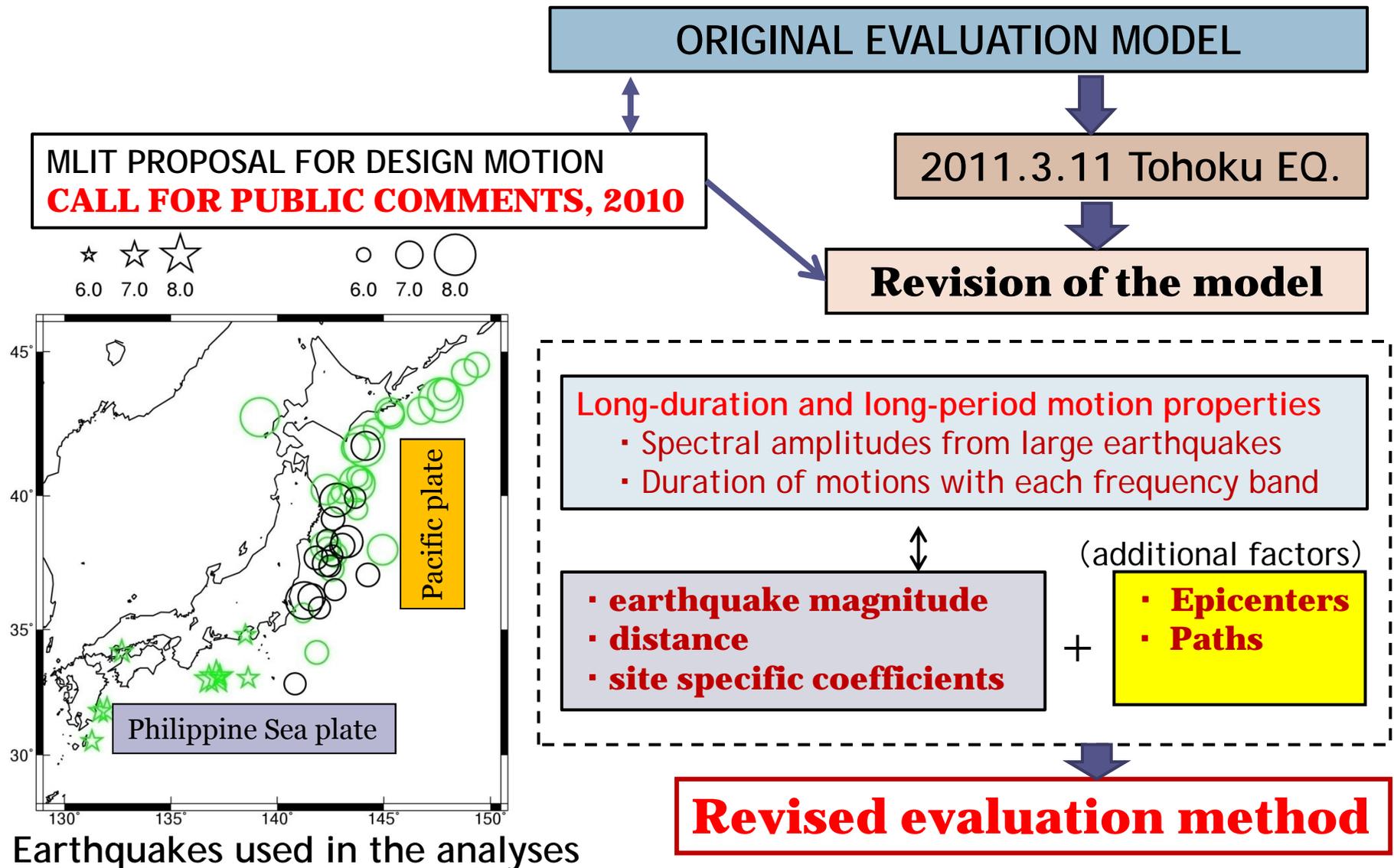
## *4. Coping Activities on Selected Issues*

# System to Revise Building Structural Codes



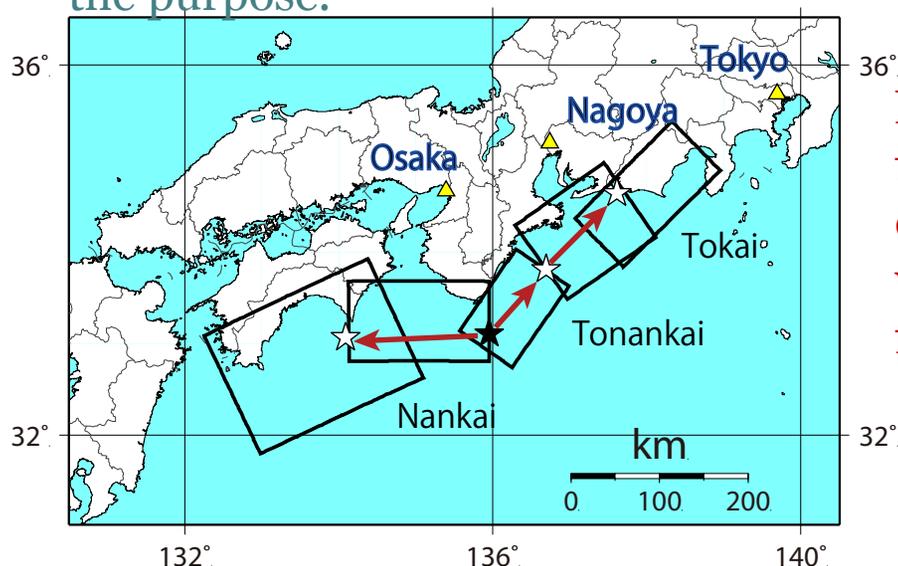
1. *Digital data by BRI strong motion network*
2. *Long-duration and long-period ground motion, structural performance under multiple cycles of loadings*
3. *Higher level of PBD, functional after earthquake*
4. *Fall down of ceilings in spatial structures and escalators in shopping centers*
5. *Fractured lead damper in seismically isolated buildings*
6. *Inclination due to liquefaction in residential houses*
7. *Evaluation of tsunami force*
8. *etc.*

*Long-duration and long-period ground motion prediction method based on observation at about 1600 stations*

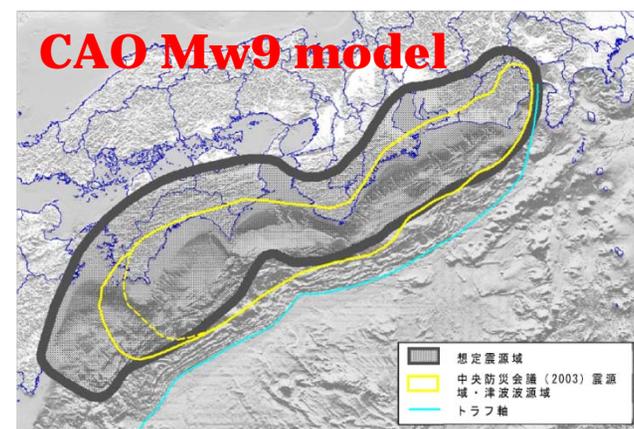
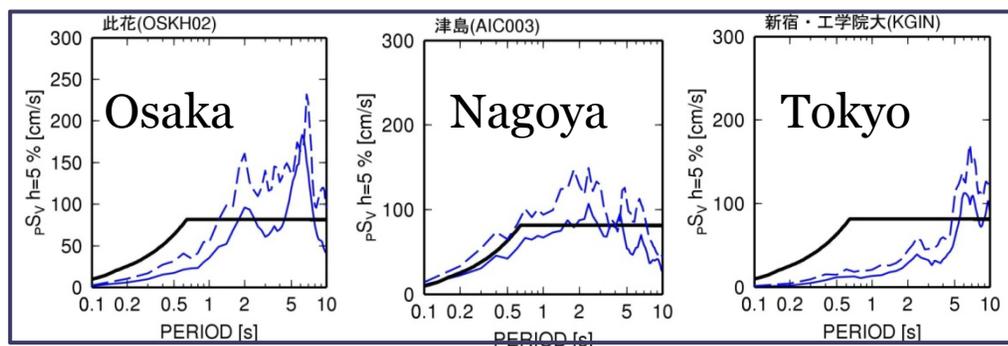
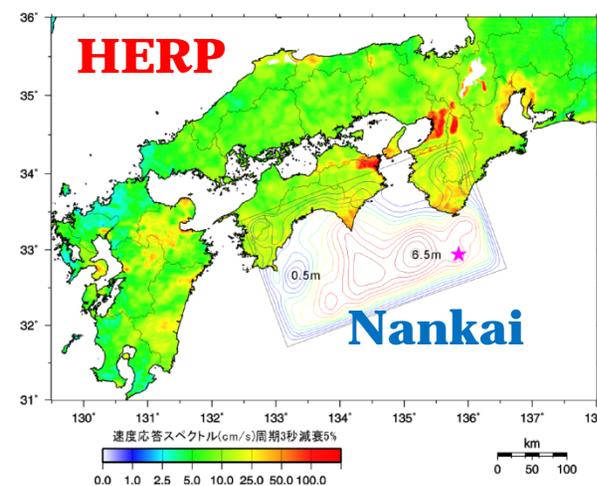


## Long-duration and long-period ground motion prediction method based on observation at about 1600 stations (cont.)

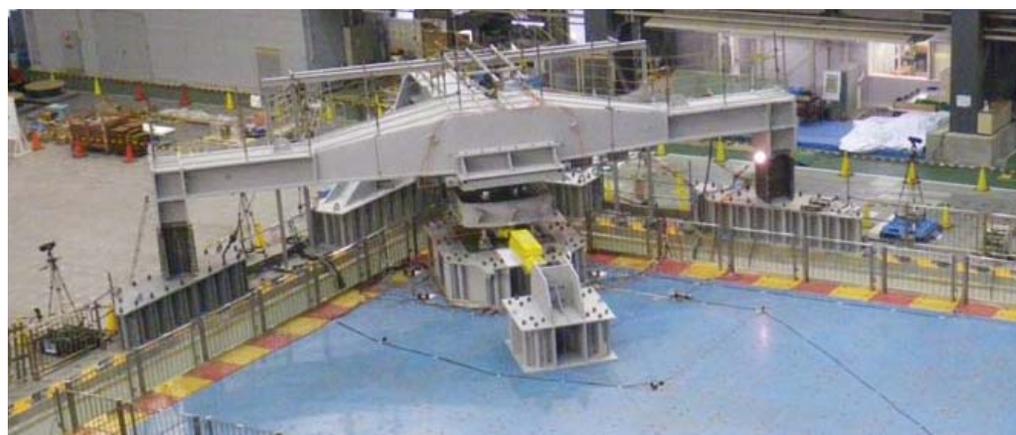
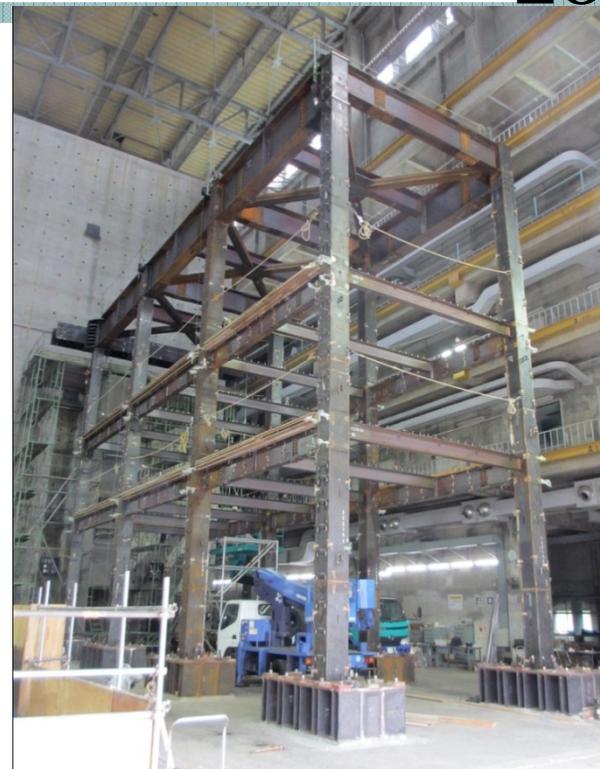
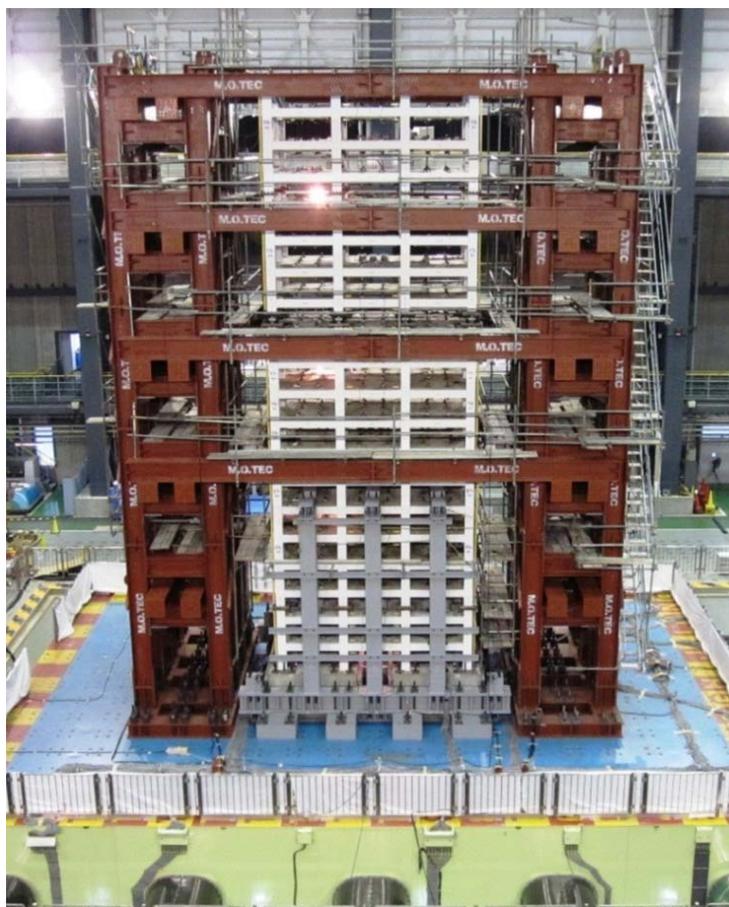
Long-duration and long-period motions were evaluated for major urban areas with two-, three- connected earthquakes, by HERP, CAO, AIJ, etc. MLIT is going to propose a design long-duration and long-period motions and is funding project for the purpose.



Nankai-trough  
three-connected  
earthquake model  
with revised model  
for major areas



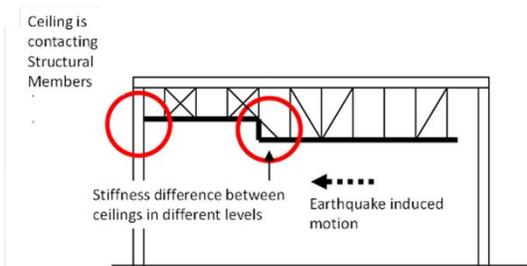
*Structural performance against long-duration and long-period ground motions (full-scale)*



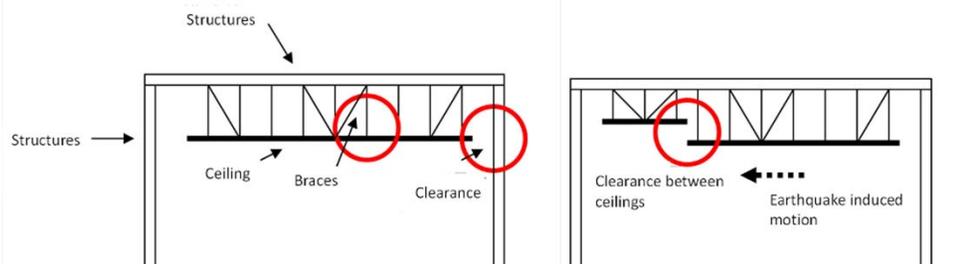
These large-size experiments are carried out under the research cooperation between the BRI and the institutions headed by Obayashi, Kajima and Taisei Co.

## Fall down of ceilings in spatial structures

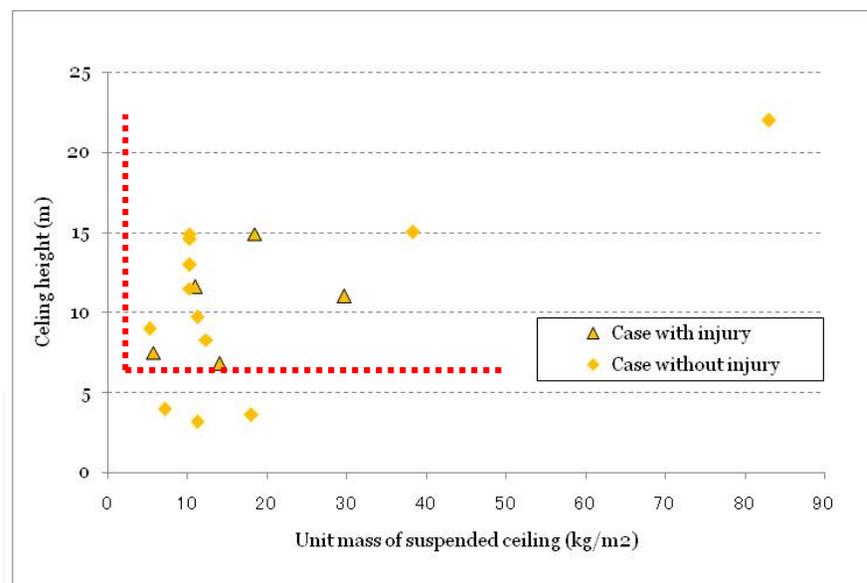
- After Geiyo earthquake (2001), a technical advice was issued to recommend putting diagonal braces on ceiling rods, and keep clearance around suspended ceiling. (see left figure)
- Construction companies reported nearly 2,000 cases of fall down of ceilings during Tohoku earthquake. Examples with/without injury are compared. (see right figure)



Frequently observed damage by earthquake



Recommended method in an MLIT technical advice



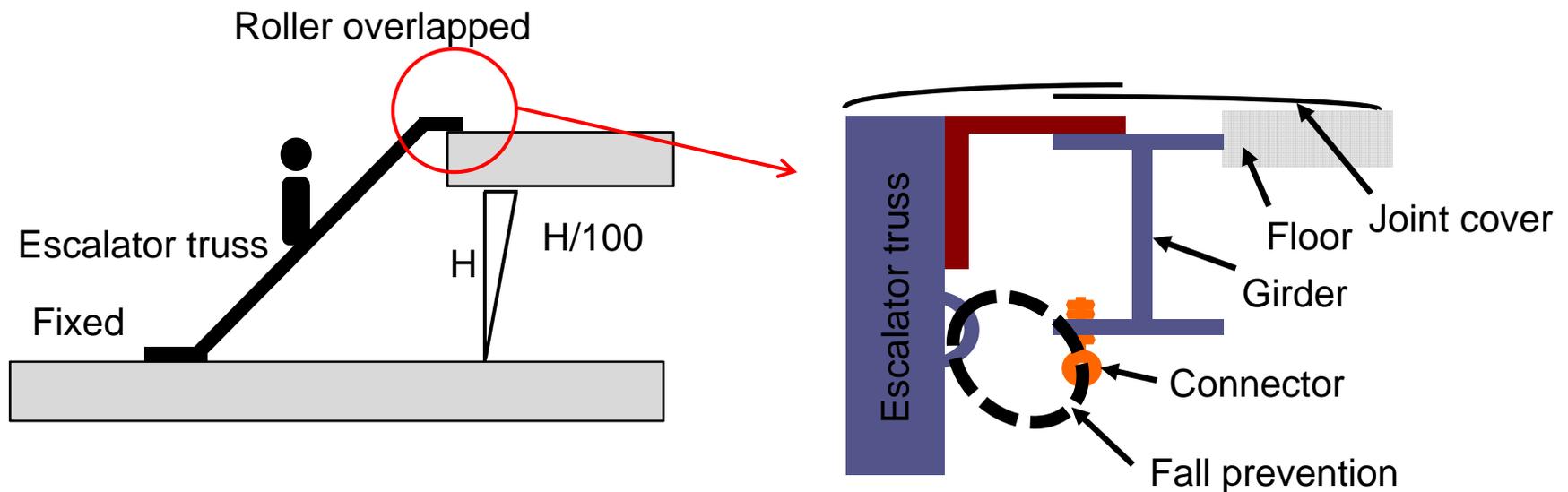
Mass and height of ceiling damaged by earthquake

## *Fall down of ceilings in spatial structures (cont.)*

- *(Tentative) Allowable Stress Design for probable earthquake + safety margin*
  - *Scope of regulation*
    - Ceiling height  $> 6\text{m}$
    - Ceiling area  $> 200\text{m}^2$
    - Unit weight of ceiling  $> 2\text{kg/m}^2$
  - *Safety margin*
    - Vertical strength
    - Clearance around ceiling

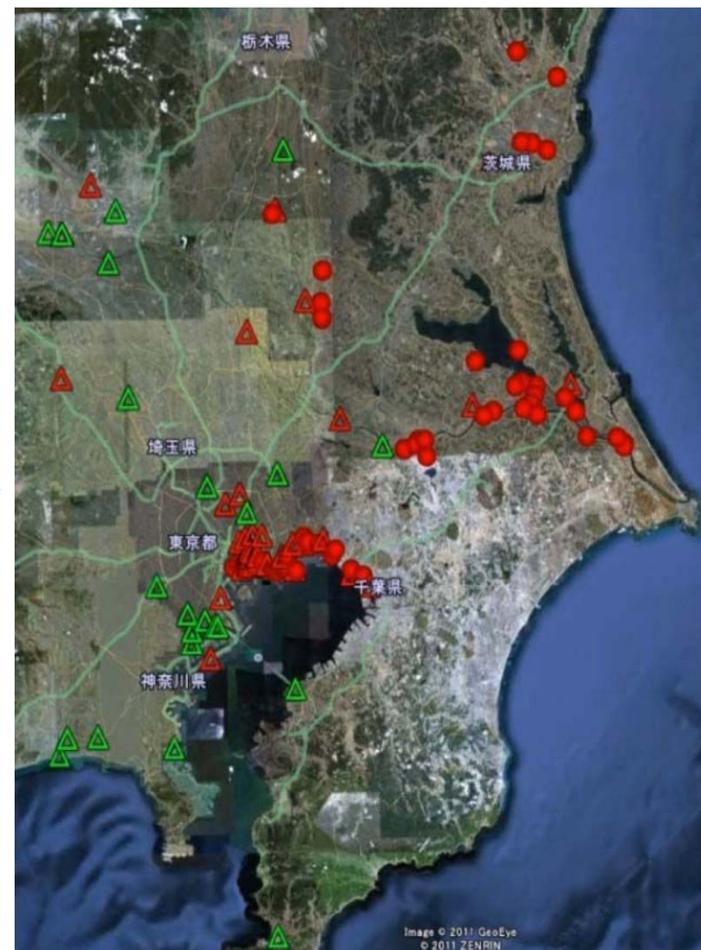
## *Fall down of escalators in shopping centers*

- *(Tentative) Requirement from  $H/100$  (current) to  $H/40$*
- *(Tentative) Exceptional relaxation to  $H/100$  in case of fall prevention device*



# Liquefaction

- Liquefaction evaluation was made by  $F_L$ -method at 112 sites in Kanto area, the results were compared with observations.
- Liquefied sites (●) are all predicted ( $F_L \leq 1$ ) but many non-liquefied sites are cautioned (△).
- Improvement of evaluation accuracy is in need.
- $F_L$ -method requires following information.
  - N-value by standard penetration test (SPT)
  - fine fraction content
  - water level
  - maximum design horizontal acceleration at surface
  - earthquake magnitude



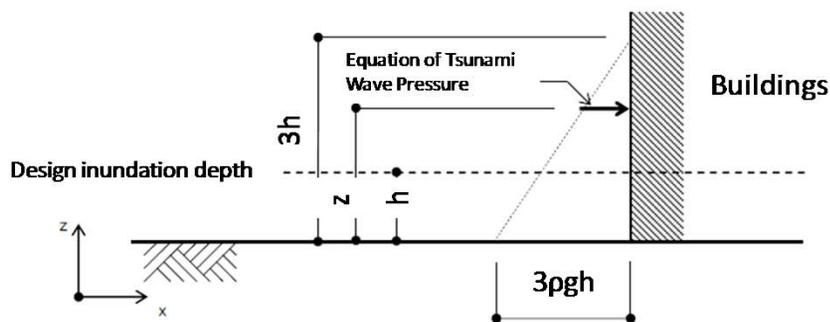
	Liquefied sites	Non-liquefied sites
$F_L \leq 1$	53 ●	35 △
$F_L > 1$	0 ●	24 △

## *Liquefaction (cont.)*

- *Japan's Building Standard Law does not require structural calculation for detached residence (residential land)*
  - Liquefaction risk is not evaluated
  - Liquefaction measures are not required
  
- *Show menus and leave selection to owners*
  - Development of affordable liquefaction evaluation method for residential land
    - BRI tries possibility of SWS (Swedish weight sounding test), plus water level and soil judgment
  - Development of practical techniques for residential land
    - Applicability to existing house
    - Prediction of subsidence

# Tsunami wave force

- Tentative guidelines for tsunami evacuation buildings -



Equation of Tsunami Wave Pressure:  $q_x = \rho g (3h - z)$

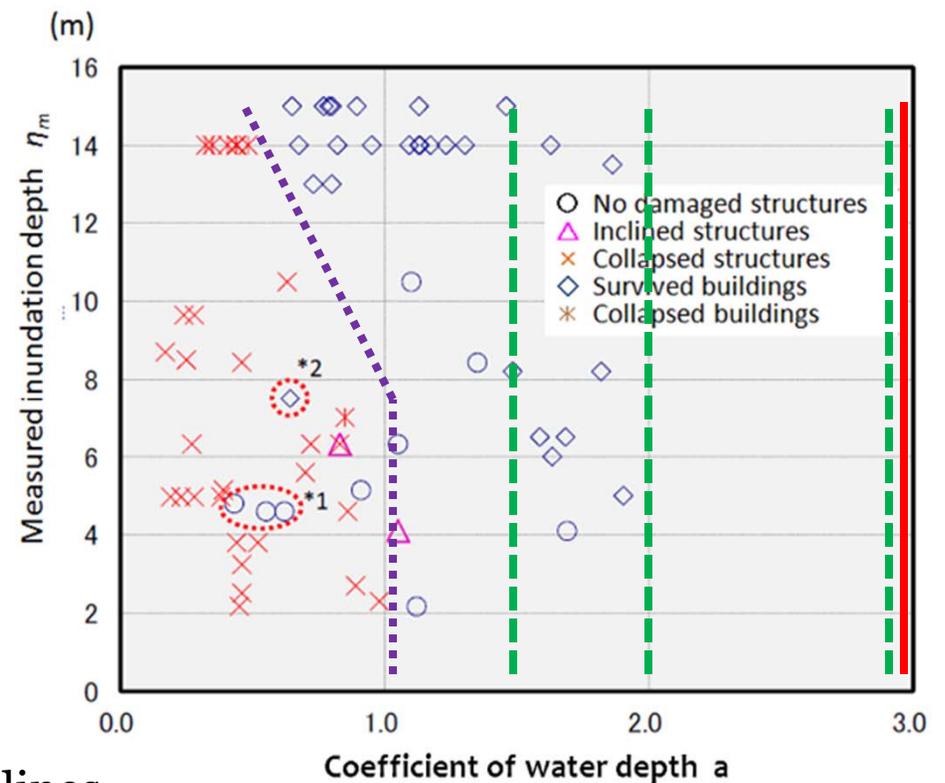
$q_x$ : design tsunami wave pressure ( $\text{kN/m}^2$ )

$\rho$ : density of water ( $\text{t/m}^3$ )

$g$ : gravitational acceleration ( $\text{m/s}^2$ )

$h$ : design inundation depth (m)

$z$ : height from the ground ( $0 \leq z \leq 3h$ ) (m)



- Previous guidelines
- - - Partially relaxed current guidelines (tentative guidelines)
- ⋯ Observed results by Tohoku Japan earthquake

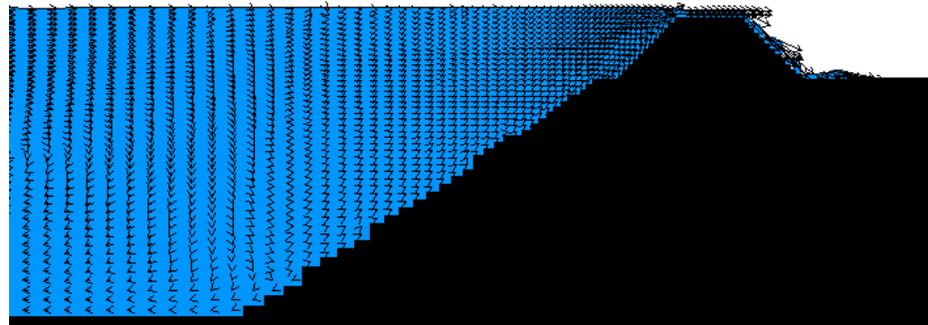
## *Tsunami wave force (cont.)*

*- Tentative guidelines for tsunami evacuation buildings -*

- BRI, Kajima Co. and U. of Tokyo have carried out waterway experiments in order to develop (improve) CFD (Computational Fluid Dynamics) technique for evaluation of tsunami pressure on buildings.*
- Improved CFD technique will be applied to evaluate the effects of openings, water infiltration, etc.*
- AIJ discusses adding new chapter of tsunami loads on buildings into “(Revised) Recommendations for Loads on Buildings” in 2014.*



Waterway experiment



Numerical simulation of Tsunami over seawall

*Thank you for your kind attention.*